June 25th, 2007 HWA Project No. 2007-094

Herrera Environmental Consultants, Inc. 2200 Sixth Avenue, Suite 1100 Seattle Washington 98121-1820

Attention:

Mr. Mark Merkelbach

Subject:

LABORATORY TESTING REPORT

& SOIL BEARING CAPACITY ESTIMATES

NOOKACHAMPS PROJECT

Dear Mr. Merkelbach:

As requested, HWA GeoSciences Inc. (HWA) performed laboratory testing for the above referenced project. Herein we present the results of our laboratory analyses, which are summarized on the attached test reports, Figures 1 through 6. The laboratory testing program was performed in general accordance with your instructions and appropriate ASTM Standards as outlined below. In addition, based upon the laboratory data developed for each soil type an estimate of the soils bearing capacity was calculated assuming the target moisture contents and densities specified by the client. The resulting bearing capacity estimates of each soil for a strip footing or a square foundation are shown on Figures 7 through 12.

SAMPLE INFORMATION: Four bulk soil samples were delivered to our laboratory on June 1, 2007, by Herrera personnel. The samples were delivered in four large plastic bags and were designated as TP-1A, TP-1B, TP-2B, and TP-3B. Visual inspection indicated that samples TP-1B and TP-2B were very similar and so those samples were combined for testing and designated TP-1B/2B.

LABORATORY COMPACTION CHARACTERISTICS OF SOIL (PROCTOR TEST): The moisture/density relationships for the three samples were determined using method ASTM D 1557 (Modified Proctor) Method C. The samples were fine grained and no correction for oversize material was required. The test results are summarized on the attached Laboratory Compaction Characteristics on Figures 1 through 3.

SHEAR STRENGTH PARAMETERS OF SOIL: Direct shear tests were conducted on each sample in general accordance with ASTM D-3080. Sample preparation included moisture conditioning the material to moisture content specified by the Client upon review of the Proctor test data. Three test specimens for each sample was prepared by remolding the soil into brass rings at the appropriate moisture content and target dry density as requested. Three shear trials were run at

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normal stresses of 2.0, 4.0 and 6.0 ksf, respectively. The results of these tests are presented on the attached reports shown on Figures 4 through 6. The apparent cohesion and friction angle of the soils are inferred from a least-squares linear regression of the three test points.

SOIL BEARING CAPACITY ESTIMATES

Bearing Capacity estimates were based on friction angle and cohesion results obtained from Direct Shear testing. For this estimate, Terzaghi's ultimate bearing capacity equation was used. Two types of footings were considered: (1) strip footing, and, (2) square footing. The depth of the footing, in both cases, was assumed to be 2 feet. A factor of safety of 3 was used to calculate the associated allowable bearing capacity.

Figures 7 through 9 represent estimates of ultimate and allowable bearing capacity for strip footing foundations with a width dimension B, and Figures 10 through 12 represent estimates of bearing capacity for square shaped footings with a side dimension of B.

These calculations assume that the fill containing the soil in question is placed in a controlled environment at a uniform density and moisture. We estimate that, when loaded, these soils will exhibit settlements of the order of 6% to 10%. A consolidation test on these soils should be performed in order to obtain more specific values for the anticipated settlement.

Based on the shear data unconfined fill slopes should be no steeper than 3H: 1V. We expect that the material can be compacted more efficiently with a heavyweight sheep foot roller. Soil placement and compaction should be monitored on a full time basis by a licensed geotechnical engineer.



CLOSURE: Experience has shown that test values on soil and other natural materials vary with each representative sample. As such, HWA has no knowledge as to the extent and quantity of material the tested sample may represent. This report should not be reproduced without the expressed written consent of the Client, and then only in its entirety. The estimate contained herein are theoretical and are for use by the client for feasibility purposes only and not for final design. Additional evaluation, including seismic and/or liquefaction potential, as well as consolidation properties need to be addressed more thoroughly. Actual bearing capacity of fill will depend on field methods used and soil conditions at the time of construction.

June 25th, 2007 HWA Project No. 2007-094

We appreciate the opportunity to provide laboratory testing services on this project. Should you have any questions or comments, or if we may be of further service, please call.

Sincerely,

HWA GEOSCIENCES INC.

George Minassian, Ph.D.

Geotechnical Engineer

Steven E. Greene, L.E.G.

Vice-President

SEG:GM:seg

Attachments:

Figures 1-3 Laboratory Compaction Characteristics of Soil

Figures 4-6 Direct Shear Test of Soils under Consolidated Drained Conditions Report

Figures 7-9 Bearing Capacity Estimates for Strip Footings

Figures 10-12 Bearing Capacity Estimates for Square Footings

LABORATORY COMPACTION CHARACTERISTICS OF SOIL



		Herrera Env		tal Const	ultants l	nc.				/AGEOS	CIENCES	INC.
		i: <u>Nookach</u>							SA	MPLE ID:	TP-1A	٩
PRO.	JECT	NO: 20070	94				mpled By: <u>(</u>			_ Tested I		
Date	Sam	pled:			Date Re	ceived: ˌ	06/07/2007	7	Da	ite Tested:	06/07/200	7
MATE	ERIA	L TYPE OR	DESCRIF	TION:						,		
Gray	brou	n CLAY with	organics									
MATE	ERIA	L SOURCE,	SAMPLE	LOCATION	DNA NC	DEPTH	:					
On si	te: T	P-1A										
Desig	natio	on: ASTM	1 D 698	Γ	XASTN	/I D 155	7	Natura	al Mois	sture Conte	ent: 41.6	%
		=						0	%	retained o	on: 3/4	in.
		<u> </u>										
Liebs	arauc	nr. LIDIY	"لک	ioist i	\allillici	.[luai	. ^	.ssumed O.	O,,	
					7	Γest Dat						
										82.3	80.1	
Moist	ure (Content (%)	30	0.3	36.	6	41.1			34.0	27.5)
	110											
				1	Annual Control	: 1		<u> </u>		Rock Correc		
	105			1 1				-	per ASTM [4718	
Method: A B X C Oversize: 0 % Preparation: Dry X Moist Rammer: X Auto Manual A Test Data Dry Density (pcf) 82.7 80.7 75.9 Moisture Content (%) 30.3 36.6 41.1	Lab Proctor	Curve										
								1				
	100		*							100% Satura	ition Line	
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_	95					: []				: 1		
<u>6</u>						-						
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		Annual Control of the										
	75							1	•		N 1 1 1 1 1	
]	10								1			
								1 1				
	70								i :			
	2	20	25	3	0	3	5	40		45		50
		Test Data y (pcf) 82.7 80.7 75.9 Content (%) 30.3 36.6 41.1										

Data Summary	*
Percent Oversize	<5%
Max. Dry Density (pcf)*	83.0
Optimum Moisture (%)*	32.0

	Test Values At Other Oversize Percentages									
0.0%	5.0%	10.0%	15.0%	20.0%	25.0%	30.0%				
83,0	85.1	87.4	89.7	92.2	94.8	97.6				
32.0	30.5	28.9	27.4	25.8	24.3	22.7				

*values corrected for oversize material per ASTM D4718, using assumed Specific Gravity shown and oversize moleture content of 1% Reviewed By:

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LABORATORY COMPACTION CHARACTERISTICS OF SOIL



CLIENT: Herrera Env	ironmental Cons	sultants Inc.		HWAGEOS	CIENCES INC.
PROJECT: Nookach	amps			SAMPLE ID:	TP-1B & TP-2B
PROJECT NO: 20070	94	Sai	mpled By: Client	 Tested	By: <i>EJB</i>
Date Sampled:		Date Received:		Date Tested:	06/07/2007
MATERIAL TYPE OR I Brown SILT	DESCRIPTION:				
MATERIAL SOURCE, On site TP-1B & TP-2E		ION AND DEPTH	[:		
Designation: ASTM	1 D 698	X ASTM D 155	7 Natura	al Moisture Conte	ent: 33.8/35.2 %
Method: A	Пв	⊠c	Oversize: 0	% retained	on: <i>3/4</i> in.
Preparation: Dry	XMoist	Rammer: X Au		Assumed S.	
		Test Da	ta		
Dry Density (pcf)	86.3	91,9	93.4	91.5	90.4
Moisture Content (%)	18.5	21.7	23.4	26.2	27.0
110				Rock Correct per ASTM D Lab Proctor 100% Satura	4718 Curve
70 10	15	20 25	5 30	35	40
		Moisture C	ontent (%)		

Data Summary	*
Percent Oversize	<5%
Max. Dry Density (pcf)*	93.4
Optimum Moisture (%)*	24.0

1	l est Values At Other Oversize Percentages									
ſ	0.0%	5.0%	10.0%	15.0%	20.0%	25.0%	30.0%			
ſ	93.4	95.5	97.7	99.9	102.3	104.8	107.4			
Ĭ	24.0	22.9	21.7	20.6	19.4	18.3	17.1			

*values corrected for oversize material per ASTM D4718, using assumed Specific Gravity shown and loversize moisture content of 1%

Reviewed By:

FIGURE 2

LABORATORY COMPACTION CHARACTERISTICS OF SOIL



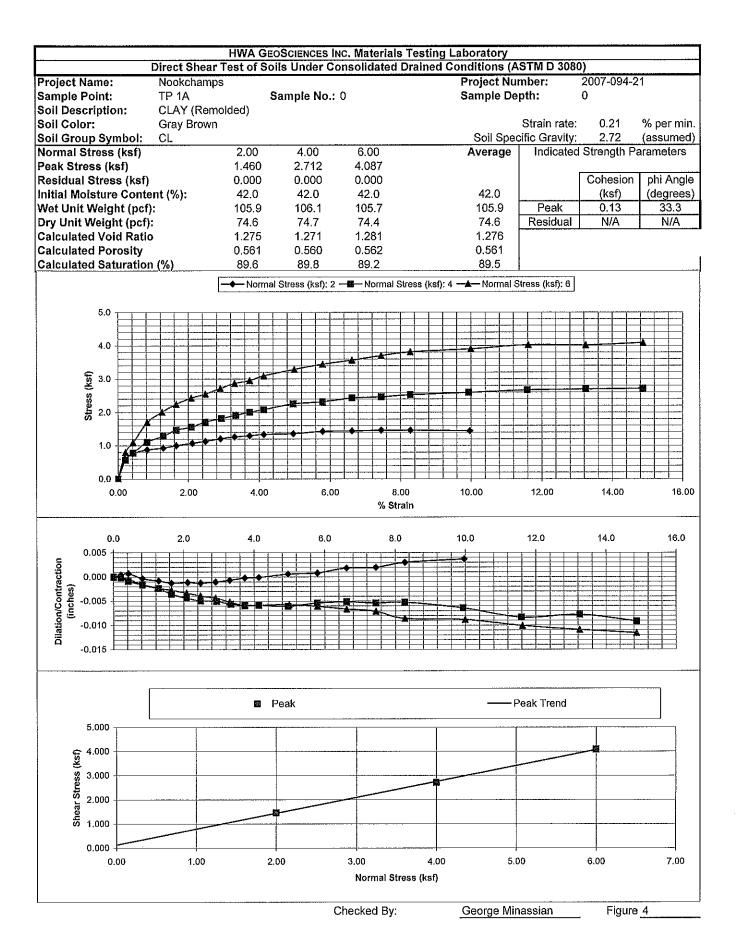
CLIENT: Herrera Environmental Cor	sultants Inc.	HWAGEOS	CIENCES INC.
PROJECT: Nookachamps		SAMPLE ID:	TP-3B
PROJECT NO: 2007094	Sampled By: <u>Clien</u>		By: <i>EJB</i>
Date Sampled:	Date Received: <u>06/07/2007</u>	Date Tested:	06/07/2007
MATERIAL TYPE OR DESCRIPTION:			
Brown, SILT with fine sand		, , , , , , , , , , , , , , , , , , , ,	
MATERIAL SOURCE, SAMPLE LOCA	TION AND DEPTH:		
On site TP-3B			
Designation: ASTM D 698	X ASTM D 1557 Natu	ıral Moisture Conte	ent: <u>42.2</u> %
Method: A B	XC Oversize: 0	% retained	on: <i>3/4</i> in.
Preparation: Dry X Moist	Rammer: X Auto Manual		
Treparation. Dry Moist	Naminor: X rate Iwandar	7100011100 0	
	Test Data		
Dry Density (pcf) 88.6	95.1 96.6	95.0	92.8
Moisture Content (%) 22.1	23.4 24.8	25.9	27.0
110			
		Rock Correc	· —
		per ASTM D	94718
105		Lab Proctor	Curve
100		•	
	-	100% Satur	ation Line
		:	
100			
6			
<u> </u>			<u> </u>
Dry Density (pcf)			
Oen Control			
λι			
90			-
85			
80			00 05
15 17 19 2°		29 31	33 35
	Moisture Content (%)		

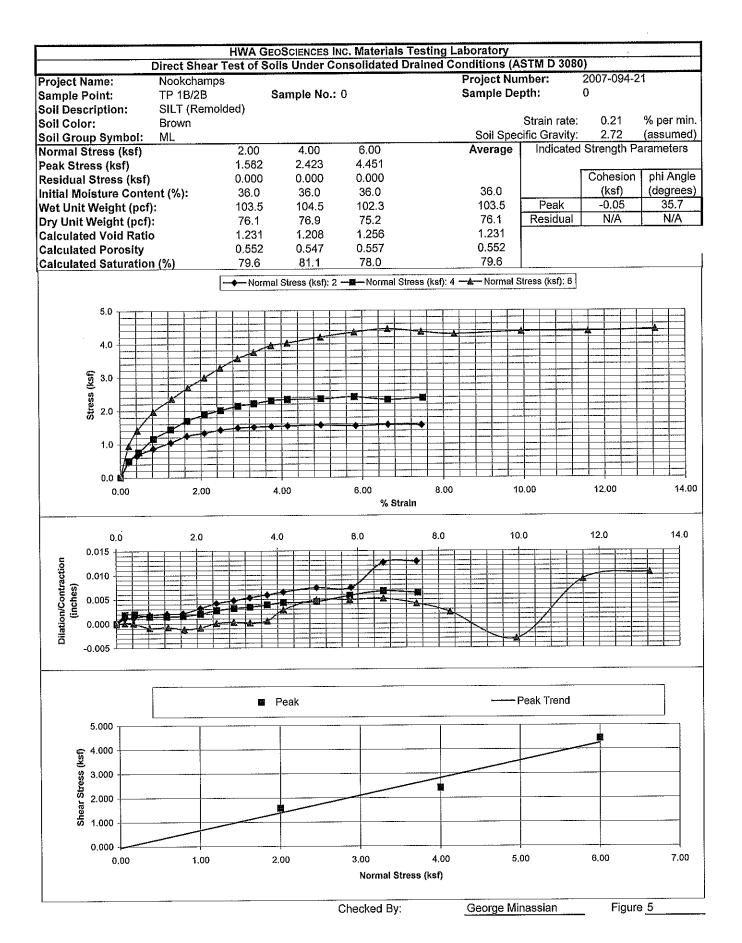
Data Summary	*
Percent Oversize	<5%
Max. Dry Density (pcf)*	96.7
Optimum Moisture (%)*	24.5

-	Test Values At Other Oversize Percentages									
	0.0%	5.0%	10.0%	15.0%	20.0%	25.0%	30.0%			
	96.7	98.8	100.9	103.1	105.5	107.9	110.5			
	24.5	23.3	22.2	21.0	19.8	18.6	17.5			

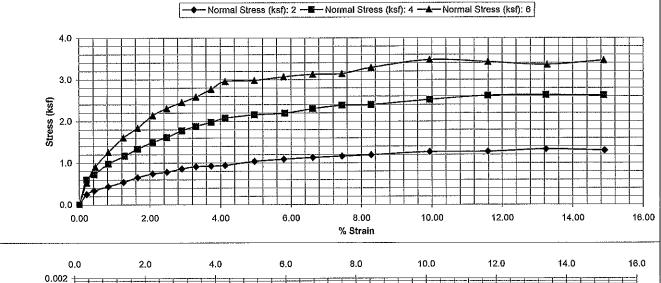
*values corrected for oversize material per ASTM D4718, using assumed Specific Gravity shown and bytersize moisture content of 1%

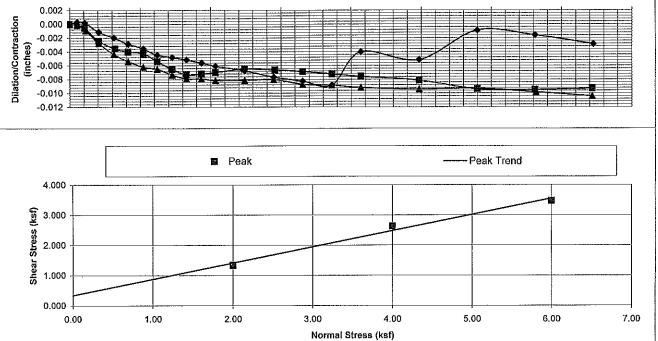
Reviewed By:





Project Name:	Nookchamps				Project Nu	mber:	2007-094-2	1
Sample Point:	TP 3B		Sample No.:	0	Sample Depth: 0			
Soil Description:	SILT (Remote	led)	-					
Soil Color:	Brown					Strain rate:	0.21	% per min
Soil Group Symbol:	ML				Soil Spec	cific Gravity:	2.72	(assumed)
Normal Stress (ksf)		2.00	4.00	6.00	Average	Indicated	Strength Pa	arameters
Peak Stress (ksf)		1.331	2.632	3.473				
Residual Stress (ksf)		0.000	0.000	0.000			Cohesion	phi Angle
Initial Moisture Conter	nt (%):	36.0	36.0	36.0	36.0		(ksf)	(degrees)
Wet Unit Weight (pcf):		102.0	102.5	102.3	102.3	Peak	0.34	28.2
Dry Unit Weight (pcf):		75.0	75.3	75.2	75.2	Residual	N/A	N/A
Calculated Void Ratio		1.264	1.253	1.256	1.258			
Calculated Porosity		0.558	0.556	0.557	0.557			
Calculated Saturation	(%)	77.5	78.2	78.0	77.9			

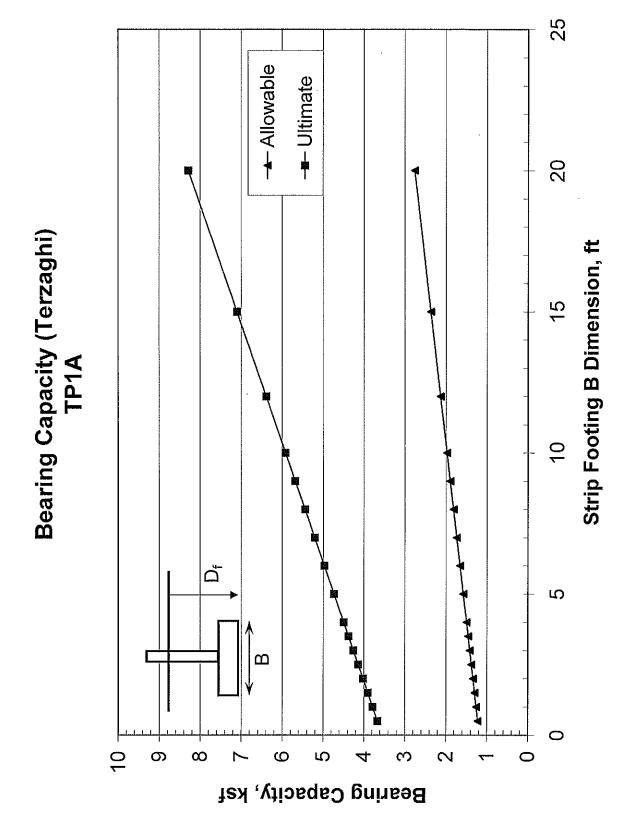




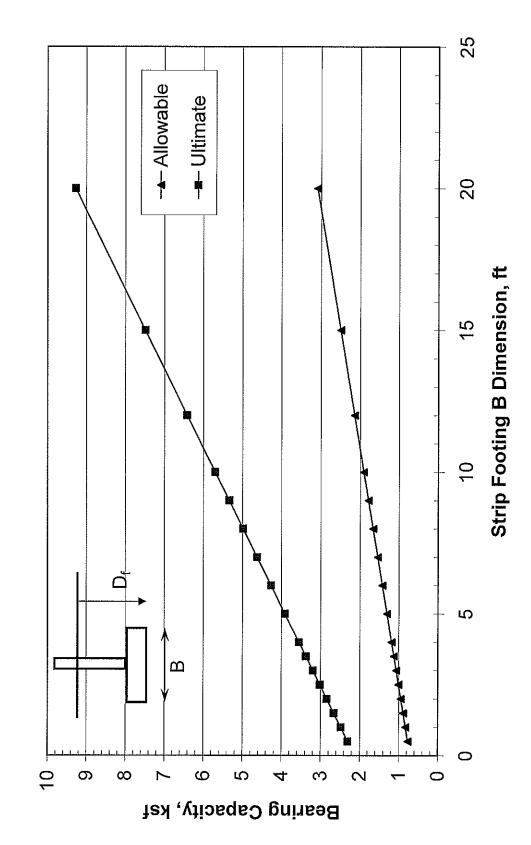
Checked By:

George Minassian

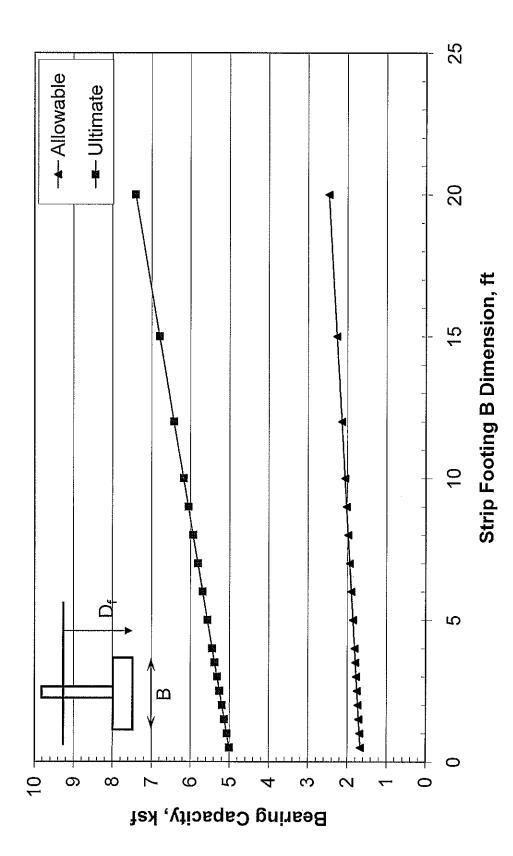
Figure 6



Bearing Capacity (Terzaghi) TP1B/2B



Bearing Capacity (Terzaghi) TP3B



→ Allowable --- Ultimate တ Bearing Capacity (Terzaghi) for Square Footing TP1A Square Footing B Dimension, ft Ŋ α 0 ന 2 Bearing Capacity, kaf 4 ∞ ⊿ ဖ

→ Allowable -■- Ultimate Bearing Capacity (Terzaghi) for Square Footing TP1B/2B 9 Ŋ Square Footing B Dimension, ft ന N ထ Ŋ ഗ 0 Bearing Capacity, ksf

